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(54) Floating ring mixer for extruder

(57) An extruder mixer has a plurality of rotor rings (28,42) provided on the downstream end of a motor driven extruder shaft (20) mounted for rotation in a conventional heated barrel (10) or stator.

The rings comprise a plurality of spaced driven rotor rings (28) spaced apart from each other and a plurality of non-driven but rotatable floating rings (42) interleaved between each pair of driven rotor rings. Both rings have

parallel upstream and downstream faces between which polymer flow passageways (44,46) extend so that the polymer melt moves downstream first through one type of ring followed by movement through the other type of ring and the viscosity of the melt causes the rotatable floating rings (42) to be rotated by the driven rings at a slower speed than the driven rings (28) so that shearing force on the melt effects mixing of the melt.

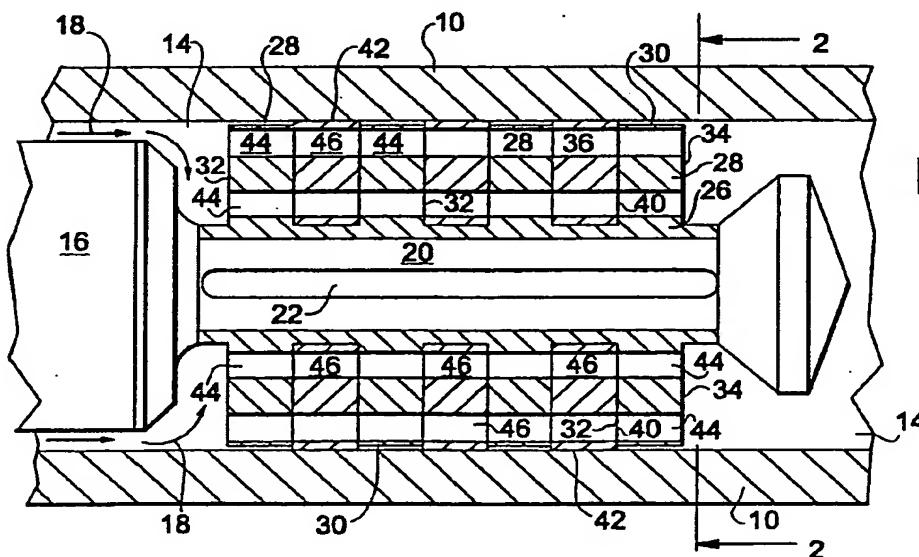


FIG. 1

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Description

BACKGROUND OF THE INVENTION

[0001] The present invention is in the field of polymer extruders and mixers for use in connection with providing high pressure polymer melts for injection moulding and extrusion and the like.

[0002] It is well known in the art to provide a polymer melt mixer in a heated extruder barrel, sometimes referred to as a stator, including a bore defining a cylindrical internal chamber in which a screw rotor is axially positioned for a rotation within and with respect to the cylindrical chamber. It is also conventional to have the upstream portion of the rotor comprise a driven rotary screw member for feeding the polymer components along the length of the rotor or barrel to a downstream portion which provides mixing of the the melted components prior to injection of the polymer melt into a die or the like. The polymer melt injection is effected by moving the rotor in a downstream direction to force the viscous polymer melt constituents from the barrel out through an opening communicating with the interior of a die or the like. A device of the foregoing type is exemplified in prior U.S. Patent No. 5,013,233.

[0003] It is extremely desirable that the polymer melt be thoroughly mixed following melting so as to achieve optimum uniformity of structure in the finished product produced by the injection molding operation. A number of different approaches have been suggested for achieving improved polymer melt mixing as evidenced by the following discussed prior art.

[0004] The Semmekrot U.S. Patent Nos. 5,013,233 and 5,158,784 disclose a dimpled downstream rotor portion having cavities 22, 23 surrounded by a mixing ring or sleeve 9 having radial openings through which the polymer melt moves to and from the rotor dimples as it works its way from the upstream to the downstream end of the apparatus. Mixing occurs between cavities 22, 23 of the rotor and mixing ring 9 which is arranged for free rotation about the rotor of the Semmekrot device. The mixing ring or sleeve nine is provided with an annular valve body 17 that coacts with a valve seat 18 on the rotor to prevent reverse flow of polymer melt in an upstream direction beyond a valve seat 18 during the injection process.

[0005] Another approach is revealed in Upmeier U.S. Patent No. 4, 541, 982 which discloses a polymer melt extruder employing multiple fixedly positioned distributing disks positioned one behind the other in alignment with each other to effect a plurality of flow dividing mixing operations. The disks are arranged as stationary structures through which melt flow occurs in serial manner.

[0006] Sato U.S. Patent No. 4, 057, 379 discloses an extruder having a driven screw type extruder screw 6 which forces melt material to be extruded through a driven rotating disk 12 having holes 14 into a stationary disk 16 having holes 26 and which is spaced from contact

with the driven rotating disk.

[0007] West German DL 0155, 504 of Elektroger dis-
closes a static mixing device for injection molding having
plurality of discs 3 having flow through apertures 4 for
producing turbulence and effecting mixing of polymer
melt. Each of the discs is separated from the next adja-
cent disc by spacers to provide chambers between the
discs. The discs and spacers are firmly clamped togeth-
er so as to prevent them from rotating relative to each
other.

[0008] British Patent No. 1,475,216 discloses a driven
cylindrical rotor cooperating with a plurality of inner and
outer profile rings for cooperation with the rotor for ef-
fecting mixing of polymer melt.

[0009] Applicant's earlier U.S. Patent No. 4,779,989
discloses a transfer mixer assembly for use with an ex-
truder screw employing a stator in which a rotor body
36 having grooves 37 and 42 is positioned for coopera-
tion in effecting mixing.

[0010] While some of the known prior art devices have
provided fairly satisfactory mixing results, there have re-
mained a number of problems including inadequate mix-
ing performance and the high cost of fabrication and
maintenance due to the complexity of some of the de-
vices.

[0011] Therefore, it is a primary object of the present
invention to provide a new and improved mixer and/or
mixer-intruder that provides enhanced mixing results, is
economical to fabricate and maintain and is reliable and
easy to use.

SUMMARY OF THE INVENTION

[0012] Achievement of the foregoing objects is ena-
bled by the preferred embodiment of the invention by
the provision of a plurality of rotor rings provided on the
downstream end of an extruder shaft mounted for rota-
tion in a conventional heated barrel or stator. The up-
stream portion of the extruder comprises a conventional
screw construction of spiral shape provided on the ex-
truder shaft which is rotated by motor means so as to
drive the polymer melt in a downstream direction toward
the rotor rings.

[0013] The rings are of two different types, namely, a
plurality of spaced driven rotor rings spaced apart from
each other along the length of an extension of the shaft
and a plurality of non-driven floating rings interleaved
between each pair of rotor rings. The rotor driven rings
are mounted on a rotor sleeve keyed to the shaft so as
to be rotated by the shaft. Both the driven rotor rings and
the floating rings have parallel upstream and down-
stream faces between which polymer flow passage-
ways extend so that the polymer melt moves first
through one type of ring followed by movement through
the other type of ring toward the downstream end of the
barrel.

[0014] The polymer flow passageways are arranged
in their respective rings in concentric circles with respect

to the axes of the shaft and the rings which are coaxial. The polymer passageways of both the driven rotor rings and the floating rings are alignable with each other, however, such alignment is only momentary since the floating rings and driven rings rotate at different speeds relative to each other. The speed differential is achieved because the floating rings have an outer periphery in the form of a cylindrical surface which contacts the inner cylindrical surface of the extrusion chamber so that there is some, but not absolute, frictional resistance to rotation of the floating rings.

[0015] In operation, the rotation of the extruder shaft results in rotation of the extruder screw and the driven rotor rings through which viscous polymer melt is forced by rotational operation of the extruder screw to move polymer melt through the polymer flow passageways of the first or upstream driven ring to enter the polymer flow passageways of a next adjacent downstream floating ring. The polymer melt passes through the polymer flow apertures of the next adjacent floating ring and into the polymer melt passageways of the second driven rotor ring which is rotating at the same speed as the first driven rotor ring which relationship adds to the rotational force applied to the floating ring. However, since the polymer melt is viscous, the rotation of the driven rings causes the viscous polymer melt to create a driving rotational force on the floating rings which is partially resisted by the frictional contact of the outer periphery of the floating ring with the cylindrical surface of the barrel in which the entire assembly is positioned. Consequently, there is relative rotary motion between the upstream driven rotor ring and the next adjacent floating rotor ring which creates a shearing force on the polymer melt to provide a substantial and effective mixing of the polymer melt so that by the time it reaches the downstream end of the mixing chamber, the polymer melt has been thoroughly mixed.

[0016] The upstream driven rotor ring is provided with a conical valve surface which during the initial portion of each cycle of operation is spaced from an identical conical valve surface on the downstream end of the screw shaft so that the space between the two conical valve surfaces comprises an annular polymer infeed aperture through which the polymer melt moves from the screw into the mixing chamber to pass through the driven rotor rings and the floating rings. However, when the shaft and the driven extruder screw begin to move toward the downstream end of the chamber to initiate an extrusion operation, the conical valve surface on the downstream end of the screw shaft moves into sealing contact with the conical valve surface on the upstream driven rotor ring to prevent back flow of polymer melt toward the screw during subsequent movement of the seals, the shaft and the rotor rings move in unison toward the downstream end of the chamber to effect discharge of the polymer melt into the die.

BRIEF DESCRIPTION OF THE DRAWINGS

[0017]

Figure 1 is a bisecting sectional view of a first embodiment of the invention illustrating the downstream end of the extruder screw and the mixing section components;

Figure 2 is a sectional view taken along lines 2-2 of Figure 1;

Figure 3 is a bisecting sectional view of a second embodiment illustrating the auger screw in its upstream position during the initial stage in a cycle of operation in which the melt polymer is being fed through an annular passageway into the rotor rings; and

Figure 4 is bisecting section view similar to Figure 3 but illustrating the auger and shaft in the closed position assumed shortly after the beginning of an injection cycle in which the annular passageway is closed by positioning of the downstream end of the auger screw against the upstream facing surface of the most upstream ring of the ring assembly.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0018] Attention is initially invited to Figure 1 of the drawings which illustrates the first, and least complex, embodiment of the invention. The primary components of the first embodiment comprise a heated barrel or stator 10 having a cylindrical bore surface 12 which defines a cylindrical chamber 14 having a longitudinal axis co-extensive with the center of cylindrical surface 12. A conventional power driven extruder screw 16 is coaxially positioned with respect to cylindrical bore 12 in chamber 14 and is rotated about its axis in conventional well known manner by power drive means (not shown). The extruder screw 16, can, for example, be of the types shown in U.S. Patent Nos. 4,779,989, 5,158,784 or 5,013,233. However, it should be understood that the invention is not limited to the foregoing types of extruder screws and a large number of conventional extruder screws and drive arrangements for same could be employed in practice of the invention.

[0019] Additionally, the extruder screw is capable of being moved to the right in the downstream direction for effecting injection of the polymer melt with such movement being effected by conventional piston means such as shown in Figure 2 of U.S. Patent No. 5,013,233. Additionally, it should be understood that rotation of the power driven extruder screw 16 effects the flow of polymer melt in the direction of arrows 18 from left to right through annular infeed opening 19 as shown in Figure 1. The left to right flow of the polymer melt is in a downstream direction and the term "downstream" means to the right and the term "upstream" means to the left as shown in Figure 1. It should also be understood that the

extruder screw includes an outwardly extending spiral screw member such as that shown in U.S. Patent No. 5, 013, 233 but which is not illustrated in the drawings for the sake of clarity.

[0020] A driven shaft extension 20 extends in the down stream direction from the downstream end of the power driven extruder screw 16 and includes a key slot 22 in which a drive key 24 is positioned. The outer portion of drive key 24 is positioned in a slot in a rotor sleeve 26 so as to effect rotation of rotor sleeve 26. A plurality of driven rotor rings 28 extend radially outward from rotor sleeve 26 in a unitary manner as shown in Figure 1. Each driven rotor ring 28 has an outer cylindrical surface spaced from cylindrical bore surface 12 of barrel 10 and an upstream face 32 and a downstream face 34. Thus, rotation of rotor sleeve 26 easily effects driven rotation of the driven rotor rings 28 in an obvious manner without any frictional drag from barrel 10.

[0021] A plurality of floating rings 36 are also provided on rotor sleeve 26 with the floating rings 36 being interleaved with the driven rotor rings 28. However, the floating rings 36 are not driven by rotor sleeve 26 but are instead mounted so as to be capable of rotation relative to rotor sleeve 26. Each floating ring 36 has an upstream face 38 which faces the downstream face 34 of an adjacent driven rotor ring 28. Similarly, each floating ring has a downstream face 40 which faces an upstream face 32 of the next adjacent driven rotor ring 28 as shown in Figure 1. Additionally, each floating ring 36 has an outer cylindrical surface 42 defining its outer periphery and lightly engaging the inner cylindrical surface 12 of the barrel or stator 10. The light engagement of surfaces 42 and 12 creates frictional resistance against rotation of the floating rings 36; however, the frictional resistance is not of great magnitude and can be overcome by the rotational movement of the polymer melt moving between each driven rotor ring 28 and adjacent floating rings 36 in a manner to be discussed. Additionally, it should be noted that there is loose clearance between the facing ring surfaces 34, 38 and 32, 40 so that there is a minimal amount of friction between rings 28 at 36 so that driven rotor rings 28 can rotate without any substantial resistance from floating rings 36.

[0022] Each of the driven rotor rings 28 is provided with a plurality of polymer flow passageways 44 which extend between their upstream face 32 and their downstream face 34 as shown in Figure 1. The polymer flow passageways 44 are arranged in three concentric circles comprising an inner circle most closely adjacent to rotor sleeve 26, an intermediate circle adjacent the inner circle and an outermost circle adjacent the outer periphery of each driven rotor ring as shown in Figure 2.

[0023] The floating rings 36 are similarly provided with polymer flow passageways 46 which can be precisely aligned with the passageways 44 of the driven rotor rings 28. However, it should be understood that relative rotation of floating rings 36 with respect to driven rotor rings 28 causes such total alignment of the polymer flow

apertures to be momentary.

[0024] In operation, the power driven extruder screw 16, driven shaft 20, drive key 24 and rotor sleeve 26 are rotated by conventional electric motor drive means and such rotation consequently results in rotation of the driven rotor rings 28 in an obvious manner. Rotation of the power driven extruder screw 16 causes polymer melt to flow in the direction of arrows 18 and into the space immediately upstream of the power driven rotor ring 28 facing the screw 16 as shown in Figure 1. The polymer melt flows into the polymer flow passageways 44 of the most upstream power driven rotor ring 28 and moves through polymer passageway 44 to enter into the polymer flow passageway 46 of the floating ring 36 immediately downstream of the most upstream driven rotor ring 28. However, the frictional engagement of the outer cylindrical surface 42 of the floating rings 36 causes some resistance to rotation of the floating rings so that the power driven rotor rings 28 consequently rotate at a greater velocity than the floating rings 36. The speed of the polymer melt is quite substantial so that the polymer melt creates rotational force on floating rings 36 sufficient to overcome the friction between surfaces 12 and 30 and causes the floating rings to rotate. However, the frictional drag between outer surface 30 of the floating rings and the barrel inner surface 12 causes floating rings 36 to rotate at a slower speed than the speed of rotation of the driven rotor rings 28.

[0025] The fact that the floating rings and the power driven rotor rings 28 rotate at different speeds results in shear forces acting on the polymer melt moving between rings 28 and 36 to effect substantial mixing of the polymer melt so that by the time the polymer melt is through mixing when it emerges from the mixing section at the downstream side of the right hand power driven rotor ring 28. The power driven extruder screw 16, shaft 20, rings 28 and 36 are all then shifted to the right by conventional drive means to effect ejection of the polymer melt from chamber 14 into an injection mold, not shown, in a well known manner. At the completion of the injection stroke, the entire extruder screw etc. assembly is then reciprocated back to the starting position to permit the initiation of a subsequent cycle of operation.

[0026] A second embodiment of the invention illustrated in Figures 3 and 4 differs from the first embodiment in that the initial movement of the power driven extruder screw 16 from its fully retracted position toward the downstream end of the barrel serves to effect closure of the annular infeed opening 19 between the extruder screw and the mixing chamber to preclude reverse flow-back of polymer melt into the extruder screw. The foregoing results are achieved by the employment of a modified floating ring 136 positioned in facing relation to a conical valve surface 152 on the downstream end of power driven extruder screw 16 instead of a driven ring as employed in the embodiment of Figures 1 and 2.

[0027] The upstream or forward face of the modified floating ring 136 includes a conical ring valve surface

150 which faces the conical through valve surface 152 as shown in Figure 3. The modified floating ring 136 includes a plurality of inner ring polymer flow passageways 146 which communicate with the next adjacent downstream ring polymer flow passageways 44 of driven rotor ring 128 which is identical to the driven rotor ring 28 of the first embodiment. The modified floating ring 136 also includes a plurality of canted polymer flow passageways 148 which communicate with the outer most ring polymer flow passageways 144 of the driven ring member 128. It should also be observed that the modified floating ring 136 also has a group of intermediately positioned polymer flow passageways aligned with the intermediate group of polymer flow passageways of the next adjacent ring but which is not illustrated in the drawings.

[0028] During the initial portion of a cycle of operation, the components are positioned so that the valve surfaces 150 and 152 are spaced from each other as shown in Figure 3. The aforementioned positioning of the valve components provides for the open annular infeed passageway 154 of annular shape between the valve surfaces which permits the inflow of polymer melt in the manner shown by the arrows in Figure 3.

[0029] When the injection phase of the cycle begins, the power driven extruder screw 16 is moved to the right so that valve surfaces 150 and 152 are forcefully engaged with each other to close annular inflow passageway 154 to prevent reverse flow of polymer melt back toward the auger during the high pressure injection operation.

[0030] In both embodiments, the flow of polymer melt through the polymer flow passageways 44 enters the passageways of the floating rings 36 to effect rotational drive to the floating ring 36 due to the fact that the driven rings are rotating faster than the floating rings. The polymer melt is consequently subjected to a shearing action due to the speed differential between the two different types of rings and the mixing of the polymer melt is consequently enhanced. If the polymer melt is of high viscosity, the speed of rotation differential between the floating ring and the driven ring will be less than it will be if the viscosity was of a reduced value. It should also be noted that discharge of the polymer melt through the passageways on the downstream side of the floating rings enters a driven rotor ring that is rotating at a greater velocity than the speed of rotation of the floating rings so that shearing mixing of the polymer melt is effected at each transfer point from the floating rings to the driven rings. Thus, the polymer melt which reaches the downstream end of the barrel is assured of being uniformly mixed.

[0031] Modifications and variations of the above-described embodiments of the present invention are possible, as will be appreciated by those skilled in the art in light of the above teachings. For example, the number of rings, the shape and number of the ring passageways and other aspects of the preferred embodiment can be

modified without departing from the spirit and scope of the invention. It is therefore to be understood that, within the scope of the appended claims and their equivalents, the invention may be practiced otherwise than as specifically described

Claims

1. A polymer melt mixer for an extruder assembly having a cylindrical bore (12) defining a cylindrical chamber (14) having an upstream end and a downstream end in which a driven extruder screw (16) is positioned for rotation about its axis to move polymer melt in a downstream direction through said chamber, said mixer comprising:

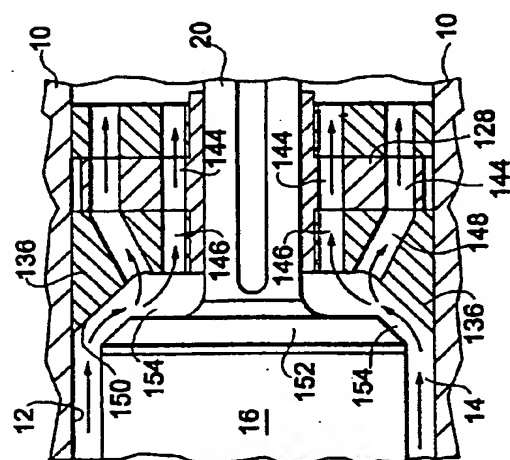
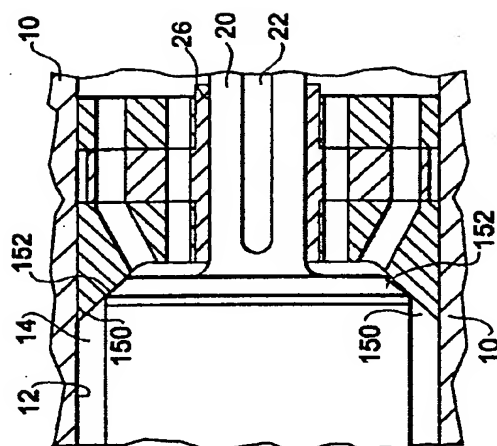
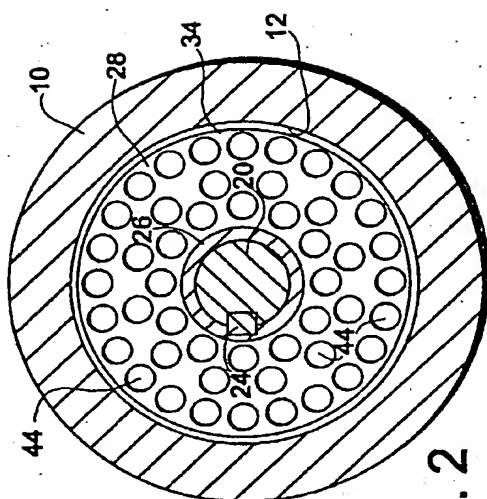
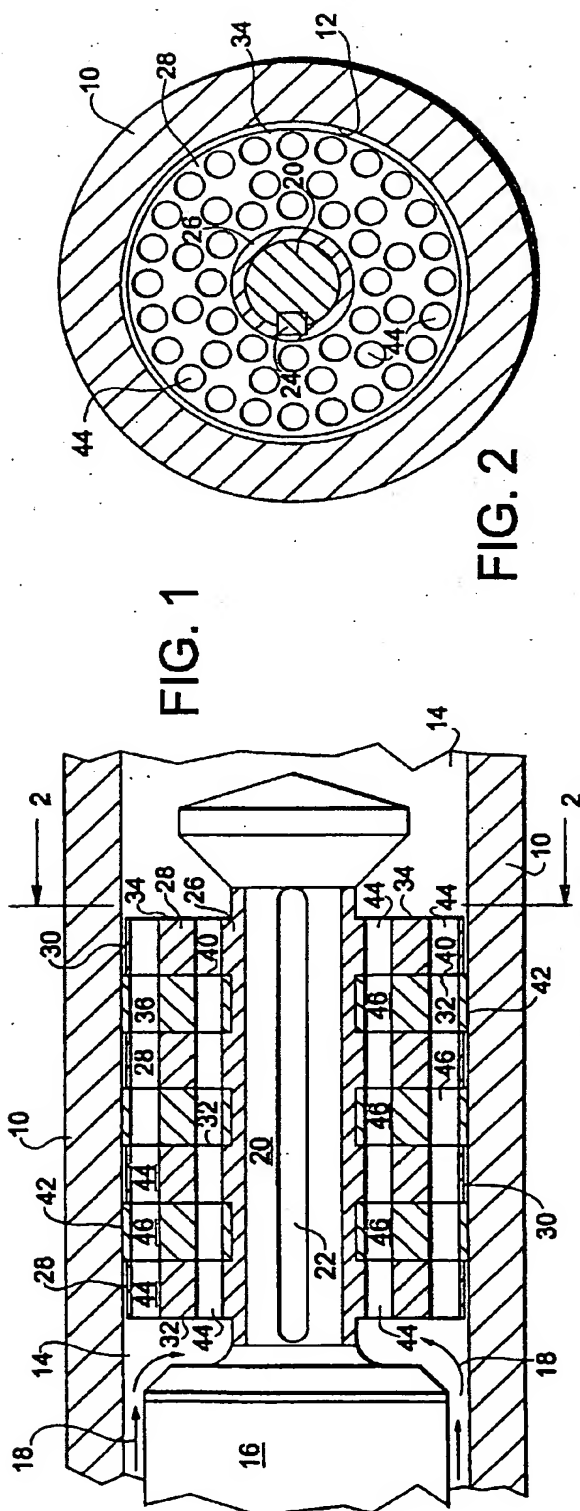
a) a plurality of driven rotor rings (28) including an upstream driven rotor ring (28) facingly adjacent the driven extruder screw (16) with each driven rotor ring (28) extending radially relative to the cylinder axis and being axially spaced from other driven rotor rings; and

b) a plurality of floating rings (36) interleaved between adjacent ones of said driven rotor rings (28), extending radially relative to the cylinder axis and capable of rotating relative to said driven rotor rings (28);

said driven rotor rings (28) and said floating rings (36) both having upstream (32,38) and downstream faces (34,40) and polymer flow passageways (44,46) extending between their upstream and downstream faces whereby polymer melt moving downstream passes through said flow passageways (44,46) and provides a driving force from the driven rotor rings (28) to effect both rotation of the floating ring (36) and mixing of the polymer melt.

2. A polymer melt mixer according to Claim 1, further comprising a driven shaft (20) drivingly rotated by said extruder screw (16) and extending downstream from said extruder screw (16) and having an axis coaxially positioned relative to said cylindrical chamber (14), with each driven rotor ring (28) being drivingly connected to said driven shaft (20) for rotation with said driven shaft and each floating ring (36) being capable of rotating relative to said driven shaft (20), whereby polymer melt moving downstream passes through said flow passageways (44,46) and provides a driving force from the driven rotor rings (28) to drivingly rotate the floating rings (36) at a speed less than the speed of rotation of the driven rotor rings while said polymer melt is being further mixed due to different speeds of rotation between the driven rotor rings and the floating rings.

3. A mixer according to Claim 2, wherein said driven shaft (20) and said driven extruder screw (16) are mounted for reciprocation between an upstream position and a downstream position, the driven extruder screw (16) having a downstream end defining a screw valve surface (152) and wherein the upstream end of one of the rotor rings (28,136) has a ring valve surface (150) facing the screw valve surface and wherein said screw valve surface (152) of the extruder screw and said ring valve surface (150) are spaced apart by an annular inflow passageway (154) when the extruder screw is in its upstream position to permit polymer melt to flow from the extruder screw through the annular passageway (154) into the ring flow passageways (44) in said one rotor ring and wherein said extruder screw (16) is mounted for axial movement toward said mixer so that said valve surface (152) of said extruder screw engages the ring valve surface (150) of said one rotor ring so that the annular inflow passageway (154) is closed so as to preclude plastic melt reverse flow through said one rotor ring (28,136) toward the extruder screw (16).
4. A mixer according to Claim 3, wherein said one rotor ring is a floating ring (136).
5. A mixer according to Claim 1, further comprising polymer melt supply means (16) providing viscous polymer melt to the front face (32) of an upstream one of said driven rotor rings (28) so that the polymer melt moves through the flow passageways (28) of the upstream one of the driven rotor rings (28) to the rear face (34) of said upstream one of the driven rotor rings (28) to engage the front face (38) of a floating rotor ring (42) immediately downstream of the upstream one of the driven rotor rings (28) to effect both rotation of the floating rotor ring (42) and mixing of the polymer melt.
6. A mixer according to any of Claims 1 to 5, wherein said floating rings (42) are frictionally engaged with said cylindrical bore (12) to create frictional resistance to rotation of said floating rings.
7. A mixer according to Claim 6, wherein said floating rings (42) have an outer peripheral surface which contacts the cylindrical bore (12) so as to create resistance to, but not preclude, rotation of the floating rings.
8. A mixer according to any of Claims 1 to 7, wherein said upstream faces (38) of the floating rings (42) have sufficient clearance from the downstream faces (34) of the driven rotor rings (28) and the downstream faces (40) of the floating rings (42) have sufficient clearance from the upstream faces (32) of the driven rotor rings (28) so that there is minimal frictional contact between the driven rotor rings and the floating rings.
9. A mixer according to any one of Claims 1 to 8, wherein said driven rotor rings (28) are unitarily formed as radial extensions of a driven rotor sleeve (26).
10. A mixer according to any one of Claims 1 to 8, wherein said driven rotor rings (28) are drivingly connected to said driven shaft (20) by a rotor sleeve (26) positioned on said driven shaft and further including drive key means (24) drivingly connecting said rotor sleeve (26) to said driven shaft (20).
11. A mixer according to any preceding Claim, wherein said flow passageways (44,46) comprise cylindrical openings each having an axis extending perpendicularly to said upstream and downstream faces of the ring in which they are provided.
12. A method of effecting mixing of a polymer melt comprising the steps of directing polymer melt through a plurality of passageways (44) in a driven moving body (28) for discharge into a plurality of passageways (46) in an adjacent non-driven body (42) mounted for rotation immediately adjacent the moving body (28) to effect rotational movement of the non-driven body (42) at a speed less than that of the moving body (28) and simultaneous shearing mixing of the polymer melt.
13. The method of Claim 12, wherein the movement of said driven moving body (28) is rotated about an axis of rotation and the movement of the non-driven body (42) effected by discharge of the polymer melt is rotation about said axis of rotation.
14. The method of Claim 12 or 13, including the further step of directing polymer melt through passageways (46) in said non-driven body (42) for discharge into a plurality of passageways (44) in a second driven body (28) rotating at a speed exceeding the speed of rotation of said non-driven body (42) to effect further shearing mixing of the polymer melt.





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EUROPEAN SEARCH REPORT

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The present search report has been drawn up for all claims			
Place of search MUNICH		Date of completion of the search 22 February 2000	Examiner Philpott, G
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**ANNEX TO THE EUROPEAN SEARCH REPORT
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